The Entrainment Influence on the Ocean Surface Layer in Tropical Latitudes

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ABSTRACT

A nonlinear, time-dependent, baroclinic model is developed for a zonally uniform, tropical, two-layer ocean on a north-south vertical section. The lower layer is infinitely deep, at rest, and at constant temperature. The dynamics of the well-mixed surface layer are described in terms of the components of horizontal mass transport, the specific mass, and the specific enthalpy. The forcing functions of the model are the zonal wind stress, the vertical entrainment of cold water from the lower layer into the surface layer, and the surface thermal energy input. The concept of entrainment forcing is based on the approach of Kraus and Turner for parameterizing the vertical motion of the seasonal thermocline.

Since zonal gradients of all quantities are neglected, the model applies only to the ocean's interior. This is rationalized by oceanographical observations. In particular, the east-west pressure gradient term is one order of magnitude smaller than the wind stress; it may be considered as an additional forcing function and, as such, absorbed in the zonal wind stress. Scale analysis reveals two time scales inherent in the model: a short scale of 0.2 day governing the mass transport equations, and a long scale of several years governing the conservation equations for mass and enthalpy. Short-term climatic fluctuations may be controlled by the latter scale.

Solutions for the steady state with Rossby number zero are presented. For wind stress and thermal energy input, simple analytic functions similar in shape to observed patterns are used. For the entrainment function three different possible distributions are investigated, all of which have an equatorial maximum attributed to strong vertical mixing in the equatorial undercurrent region. The principle responses of the model are: 1) a meridional pattern of zonal mass transport exhibiting the main observed features, particularly an equatorial counter-current; 2) a thickness of the mixed layer similar to the observations; and 3) a surface temperature profile with an equatorial minimum. The tendency of this model to develop an equatorial counter-current is caused by the entrainment forcing. It is shown that entrainment and energy balance are not entirely independent of one another.

1. Introduction

Kraus and Turner (1967) and Turner and Kraus (1967) have presented a one-dimensional parameterization of the seasonal thermocline in the ocean, in terms of both a laboratory and a mathematical model. Their work was based on the finding of Rouse and Dodu (1955) that a density discontinuity surface in a fluid can be shifted by a vertical mass flux.

In the experiments of Rouse and Dodu the upper layer of a stably stratified two-layer fluid was constantly stirred, whereas the lower layer was at rest. The input of small-scale turbulent kinetic energy into the upper layer caused vertical mixing; the lower layer became entrained into the upper layer. The density discontinuity did not tend to become smeared but remained sharp and well-defined. The authors described the entrainment process in terms of a moder-

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The simplest possible model to do this seems to be a two-layer ocean on a north-south section with the lower layer at rest. In our model this is achieved by setting the pressure gradient equal to zero in the lower layer and by assuming that the stress at the interface affects only the upper layer. These conditions filter out the barotropic mode of motion (O’Brien and Reid, 1967). Therefore, the motion of the upper layer exhibits a baroclinic response.

We neglect the zonal derivatives of all quantities, retaining only meridional gradients. Hence the model is applicable only to the interior ocean region; sidewall effects are not taken into account. It seems that meridional oceanic boundaries are not crucial for the dynamics of this model. To rationalize this, we may restrict ourselves to some remarks about the zonal pressure gradient which does not vanish in the actual ocean. The zonal pressure gradient term would enter the zonal mass-transport equation in the approximate form

$$\int_{i}^{s} \frac{\partial p}{\partial x} \approx g \frac{\partial h_1}{\partial x},$$

(1.1)

where \( h_1 \) is the thickness of the upper layer and \( \Delta \rho \) the density difference between it and the lower layer; a complete list of symbols is given in the Appendix. Employing \( \Delta \rho = 10^{-3} \text{ gm cm}^{-3}, h_1 = 10^4 \text{ cm}, \text{ and } \partial h_1 / \partial x = 10^{-4} \text{ for the mixed surface layer, the right-hand side of Eq. (1.1) becomes } 0.1 \text{ dyn cm}^{-2}, \text{ which is one order of magnitude smaller than the zonal wind stress. Moreover, this zonal pressure gradient term (1.1) is practically independent of latitude and longitude in the interior of the Pacific Ocean. On the other hand, since meridional gradients of the mixed layer thickness are of the order \( \partial h_1 / \partial y = 10^{-4} \), the associated pressure gradient term has the same order as the wind stress. These estimates are based on oceanographical observations involving the depth of the 24.40 \( \sigma_T \)-surface\(^3\) of the Pacific Ocean (Barkley, 1968). If we now treat the zonal pressure gradient as a forcing function, we can absorb it into the zonal wind stress; therefore, the forcing function \( \tau \) introduced in the following shall be interpreted as the sum of the zonal pressure gradient and the zonal wind stress, though we will call it simply the wind stress.

The characteristics of the model are shown in Fig. 1. The entrainment process which tends to deepen the thermocline is counterbalanced by the mass flux divergence in the upper layer which otherwise is treated like a slab. The poleward mass flux out of the slab is closed by subsidence processes in high latitudes which finally carries the water masses back into tropical regions (dashed arrows). However, the present model is considered to be independent of the particular kind of recirculation mechanism.

\(^3\) Along the 24.40 \( \sigma_T \)-surface the density of the ocean water would have the constant value 1,02440 gm cm\(^{-3}\) for zero pressure.
for the specific mass of the upper layer and
\[ E = \rho h c_p (\theta_1 - \theta_0) = Q g a \partial_1 \] (2.7)
for the corresponding enthalpy, where
\[ a = c_p / (g a). \] (2.8)
The pressure term (2.5) then becomes
\[ P = \frac{1}{\rho_0} \frac{\partial}{\partial y} \left( \frac{Q E}{2} \right). \] (2.9)

The term “specific” in the present text refers to a column of unit horizontal area in the upper layer. The quantity \( a \) has the dimension of a length of the order 3000 km, corresponding to the meridional length scale of the model (see Section 3).

We now introduce the horizontal mass transport components
\[ M = \int_t \rho u dz, \quad N = \int_t \rho v dz, \] (2.10)
and replace the function \( v \) in the nonlinear terms of Eqs. (2.1) and (2.2) by its vertical average
\[ \bar{v} = \frac{1}{\rho_t h_m} \int_t \rho v dz = N / Q. \] (2.11)

The approximation (2.11) is equivalent to neglecting the correlation terms \( u'v', \bar{v}' \), where the bar operator denotes a vertical mean. We finally parameterize the interface stress vector by
\[ \left( \tau_x, \tau_y \right) = k \left( \begin{array}{c} M \\ N \end{array} \right). \] (2.12)

With Eqs. (2.9)–(2.12), the mass-transport equations take on the forms (2.14), (2.15) given below.

The continuity equation, vertically integrated over the slab, yields
\[ \frac{\partial M}{\partial y} + \frac{\partial N}{\partial t} = \frac{\partial}{\partial y} \left( \frac{Q E}{2} \right). \] (2.13)

where \( w^* \) denotes the entrainment velocity. If \( w^* > 0 \), the internal interface is shifted downward. Since the horizontal slopes of density discontinuities in the ocean on a global scale are not bigger than \( 10^{-4} \), one can neglect the horizontal component of the entrainment velocity. The entrained water does not affect the equations of the total mass transport of the slab because it carries no momentum with itself. However, it affects the continuity equation (2.13) by acting as a mass source. Likewise, it would affect the equations of the average velocity in the slab, because the entrained water has to be accelerated at the expense of this average velocity; this is the reason why we prefer to use integrated mass transport equations instead of mean

momentum equations. The magnitude of \( w^* \) is of the order \( 5 \times 10^{-4} \text{ cm sec}^{-1} \) (compare, e.g., Overstreet and Rattray, 1969). We shall call the quantity \( \rho_0 w^* \) the entrainment mass flux \( \sigma \).

In order to close the system, we add Eq. (2.17) for the specific enthalpy \( E \) of the slab; \( \xi = \xi(y, t) \) is the net thermal energy flux into the sea surface (algebraic sum of radiation balance, sensible and latent heat flux). The entrained water does not affect the specific enthalpy because the reference temperature for \( E \) is just the temperature of the lower layer. The final set of model equations is now

\[ \frac{\partial M}{\partial y} + \frac{\partial N}{\partial t} = \beta y N + \tau - k M, \] (2.14)

\[ \frac{\partial N}{\partial y} + \frac{\partial M}{\partial t} = -\beta y M - \frac{1}{\rho_0} \frac{\partial}{\partial y} \left( \frac{Q E}{2} \right) - k N, \] (2.15)

\[ \frac{\partial Q}{\partial t} + \frac{\partial N}{\partial y} = \sigma, \] (2.16)

\[ \frac{\partial E}{\partial t} + \frac{\partial N}{\partial y} = \xi. \] (2.17)

3. Scale considerations

We shall now perform a simple scale analysis. Using the nondimensionalization notations
\[ M = M' m', \quad N = M' n', \quad Q = Q' q', \]
\[ t = T' t', \quad y = Y' y', \quad E = E' e', \]
\[ \tau = D' \tau', \quad \sigma = S' \sigma', \quad \xi = Z' \xi', \]
the mass transport equations become
\[ \frac{\partial m'}{\partial t'} + \text{Ro} \frac{\partial}{\partial y} \left( \frac{n' m'}{q'} \right) = y' n' + \epsilon t' - \gamma m', \] (3.2)

\[ \frac{\partial n'}{\partial t'} + \text{Ro} \frac{\partial}{\partial y} \left( \frac{n' n'}{q'} \right) = -y' n' - \delta e' \frac{\partial}{\partial y} \left( \frac{q' e'}{2} \right) - \gamma n', \] (3.3)

with
\[ T' = 1 / (\beta Y'), \quad \text{Ro} = M' / (\beta Y' q'), \]
\[ \epsilon = D' / (\beta Y' M'), \quad \gamma = k / (\beta Y'), \]
\[ \delta = H' / Y', \quad \kappa = (a Y' M') / E'. \] (3.4)

The term \( H' \) denotes the scale of the thickness of the upper layer, i.e.,
\[ H' = Q' / \rho_0. \] (3.5)

We shall try to relate all scale of the model to the scales of the forcing functions. The latter may be given by

Wind stress: \( D' = 1 \text{ dyn cm}^{-2} \)

Entrainment: \( S' = \rho_0 \times 5 \times 10^{-4} \text{ cm sec}^{-1} \)

Energy input: \( Z' = 5 \times 10^{-4} \text{ cal cm}^{-2} \text{ sec}^{-1} \)
values which may be compared, for example, with those of Hellerman (1967), Overstreet and Rattray (1969) and Sellers (1965). For the a priori given geometrical scale we find by inspection that

$$Y' = (D'/\beta S')^{1/3} = 3 \times 10^8 \text{ cm}.$$  

(3.7)

Hence, the time scale, defined in (3.4), may be expressed by

$$T' = (S'/\beta D')^{1/3} \approx 0.2 \text{ day}.$$  

(3.8)

As $D'/S'$ has the dimension of a velocity of the order $10^4 \text{ cm sec}^{-1}$, Eqs. (3.7), (3.8) are in accordance with the scaling of Matsuno (1966) for equatorial latitudes. We shall interpret the expression (3.7) by rewriting it in the form $\beta S' Y' = D'/Y'$ which, anticipating Eq. (3.9), corresponds to the scaling of the Sverdrup transport in terms of the horizontal wind-stress gradient.

We require the forcing function of the mass transport equations (the wind stress) to be unity, i.e., $\epsilon = 1$; this results in

$$M' = (S'D'/\beta) = S'Y'.$$  

(3.9)

Likewise, we require the pressure gradient term in Eq. (3.3) to be of order unity which stipulates equality of the aspect ratio $\delta$ and the parameter $\kappa$ leading to

$$\rho_0 Y' \delta S' = Q' E',$$  

(3.10)

where equality of the two length scales $a$ and $Y'$ has been assumed. Eq. (3.10) relates the two scales $Q', E'$ to externally given quantities. In order to gain a second relation for $Q', E'$, we assume that the time scales of the continuity equation (2.16) and the thermal energy equation (2.17) may be determined by the respective source functions $\sigma$, $\xi$, and we stipulate that these time scales are equal. This eliminates the time scale and yields

$$Q'/E' = S'/Z'.$$  

(3.11)

Combining Eqs. (3.10) and (3.11), we find

$$Q' = \left(\frac{\rho_0 D' a^3}{\beta Z'}\right)^{1/3},$$  

(3.12)

$$E' = \left(\frac{\rho_0 D' a^3}{\beta S'^2}\right)^{1/3}.$$  

(3.13)

We note that this scaling of $Q'$ and $E'$ is independent of the relation (2.7) between $Q$ and $E$; however, we are led back to (2.7) by inserting the values of Eq. (3.6) into (3.11). In so doing we have

$$E' = (Z'Q')/S' = Q' \times c_p \times 10K.$$  

(3.14)

The order of the horizontal mass transport is

$$M' \approx \rho_0 \times 10^4 \text{ cm}^2 \text{ sec}^{-1},$$  

(3.16)

which corresponds to an average horizontal velocity of the order 1 cm sec$^{-1}$. Combining (3.4) for $\kappa$ with Eqs. (2.7), (3.7) and (3.9), we find

$$\kappa = \delta R_0^{-1} \text{ Fr}, \quad \text{Fr} = (M'/Q')^{1/2} (g'H'),$$  

(3.17)

where $g' = g \theta_1$ is the reduced gravity. The parameter $\epsilon$ should be understood as a Rossby number based on the wind stress (Pedlosky, 1969). However, it is not a free parameter in the present model.

The time scale $T_1'$ of the continuity and thermal energy equations, typically much larger than $T'$, was assumed to be determined by

$$T_1' = Q'/S' = E'/Z' \approx 2 \times 10^8 \text{ sec}.$$  

(3.18)

It might be interesting to note that this time constant of some 6–7 years seems to govern short-term climatic fluctuations of the tropical Hadley cell due to atmosphere-ocean interactions (Namias, 1969). We now see by combining Eqs. (3.4), (3.9) and (3.18) that

$$R_0 = T'/T_1' \approx 10^{-4}.$$  

(3.19)

Thus, the continuity and thermal energy equations take on the dimensionless forms (3.22) and (3.23), respectively. The nondimensional equations of the model are

$$\frac{\partial m'}{\partial t'} + \frac{\partial}{\partial y'} \left( n' m' \right) = \gamma' \sigma + \gamma - \gamma m',$$  

(3.20)

$$\frac{\partial n'}{\partial t'} + \frac{\partial}{\partial y'} \left( n' n' \right) = -\gamma m' - \frac{\partial}{\partial y'} (q' e'/2) - \gamma n',$$  

(3.21)

$$\frac{\partial q'}{\partial t'} + R_0 - n' = R_0 \sigma',$$  

(3.22)

$$\frac{\partial e'}{\partial t'} + R_0 - n' e'/q' = R_0 \sigma'.$$  

(3.23)

Forcing functions are the wind stress $\tau'$, the entrainment transport $\sigma'$, and the energy input $\xi'$. Parameters of the model are the Rossby number $R_0$ and the friction number $\gamma$, the latter having the approximate magnitude $0.1$.

We shall briefly relate the present model to Stommel's (1948) original approach of a nondivergent ocean. Let us consider the vorticity equation obtained from Eqs. (3.20) and (3.22) for the stationary state without advection but with entrainment; in this case, we have

$$n' = \text{curl} \, \tau' - \gamma e' - \gamma \text{curl} \, \mathbf{m}'.$$  

(3.24)

In (3.24) curl denotes the two-dimensional operator which is a scalar.
4. Analytic solution for the steady state

The special case of Eqs. (3.20)–(3.23) in which the motion is steady and the advective terms in the momentum equations vanish is described by

\begin{align*}
0 &= y' m'' + r'(y') - \gamma m', \\
0 &= -y' m' - \frac{\partial}{\partial y' \left( \frac{q' e'}{2} \right)} - \gamma n', \\
\frac{\partial n'}{\partial y'} &= \sigma'(y'), \\
\frac{\partial}{\partial y'} \left( \frac{n' e'}{q'} \right) &= \xi'(y').
\end{align*}

This set of equations is nonlinear. However, it can be solved by simple integrations of the form

\begin{align*}
n'(y') &= \int_0^{y'} \sigma'(y^*) dy^*, \\
m'(y') &= \frac{1}{\gamma} \left[ y' n'(y') + r'(y') \right], \\
q'(y') &= \left\{ q_0 e_0 - 2 \int_0^{y'} \left[ y^* m'(y^*) \\
&+ \gamma n'(y^*) \right] dy^* \right\} n'(y') \int_0^{y'} \xi(y^*) dy^* + \gamma n'(y') \int_0^{y'} \xi(y^*) dy^*, \\
e'(y') &= \frac{q'(y')}{n'(y')} \int_0^{y'} \xi(y^*) dy^*,
\end{align*}

with the boundary conditions

\begin{align*}
n'(0) &= 0, & q'(0) &= q_0, & e'(0) &= e_0.
\end{align*}
where \( q_0 \) and \( \varepsilon_0 \) are not independent of one another. Both (4.7) and (4.8) lead to indeterminate expressions for \( \gamma = 0 \). However, employing l'Hospital's rule, we find

\[
e_0' = -\frac{\zeta'(0)}{\sigma'(0)} q_0'. \tag{4.10}
\]

The argument \( \gamma' \) varies from \( \gamma' = 0 \) (equator) to \( \gamma' = 1 \) (30° latitude). There is no singularity in the solution for \( q' \) as long as the latitudinal integral of the energy balance \( \zeta' \) does not vanish (except for \( \gamma' = 0 \)); this is valid for the observed energy balance (Sellers, 1965). Likewise, there is no singularity in the solution for \( \varepsilon' \) as long as \( n'(\gamma') \) does not vanish (except for \( \gamma' = 0 \)); this is also valid because we assume the entrainment function \( \sigma'(\gamma') \) to be maximum at the equator and nowhere negative.

An important aspect of the stationary model (4.1)-(4.4) is the fact that the forcing functions \( \sigma'(\gamma') \) and \( \zeta'(\gamma') \) are not entirely independent of one another. Assume, for example, that there is no entrainment at all, i.e., \( \sigma'(\gamma') = 0 \). This causes a pattern \( n'(\gamma') = 0 \) which would not be consistent with an arbitrary profile \( \zeta'(\gamma') \neq 0 \). Conversely, if one prescribes an entrainment distribution \( \sigma'(\gamma') \neq 0 \) with \( n'(1) > 0 \), it would not be consistent to set \( \zeta'(\gamma') = 0 \). Both cases may be formally verified by inspection of Eqs. (4.3) and (4.4). They can also be interpreted from obvious physical reasons.

can develop. Obviously, the first case considered here is the trivial case mentioned in Section 3.

We shall now discuss three special examples of the solutions just obtained. For \( \tau' \) and \( \zeta' \) we choose analytical latitudinal profiles similar in shape to the observed distributions [cf. Hellerman (1967) for the stress and Sellers (1965) for the energy balance], i.e.,

\[
\tau'(\gamma') = -0.15 - 0.85 \exp[-2(3\gamma' - 2)^2], \tag{4.11}
\]

\[
\zeta'(\gamma') = 0.5(1 + \cos 2.8\gamma'),
\]

\[-0.4 \exp[-1.6(3\gamma' - 3)^2]. \tag{4.12}\]

Fig. 2 shows these two forcing functions.

No direct observations are available for the entrainment function. There is some evidence, however, that vertical mixing reaches maximum intensity in equatorial latitudes due to the equatorial undercurrent (Knauss, 1963). For this reason we shall investigate the response of the steady model to three different \( \sigma' \) distributions which are Gaussian functions centered on the equator. We use the form

\[
\sigma'(\gamma') = \sigma_0 \exp \left[ -0.69 \left( \frac{\gamma'}{\gamma_1} \right)^2 \right], \tag{4.13}
\]

where the half-widths of these functions are \( \gamma_1 = 3^\circ, 6^\circ \) and 12° latitude; we will refer to them as \( \sigma_1' \), \( \sigma_2' \) and \( \sigma_3' \), respectively (Fig. 3). Appreciable values of \( \sigma' \) are restricted to the immediate vicinity of the equatorial undercurrent region, whereas \( \sigma_3' \) exhibits a much broader distribution, though a weaker, influence of entrainment. The \( \sigma' \) functions are normalized in order to always produce the same latitudinal mass transport \( n'(1) \) across the poleward boundary (Fig. 4).

We note again that the function \( n' \) is not influenced by the wind stress [Eq. (4.5)]. Therefore, \( n' \) has nothing to do with the meridional Sverdrup transport.

![Fig. 4. Latitudinal profiles of north-south horizontal mass transport \( n'(\gamma') \) due to entrainment.](image)

![Fig. 5. Latitudinal profiles of east-west horizontal mass transport \( m'(\gamma') \) due to wind stress and entrainment.](image)
Fig. 6. Latitudinal profiles of specific mass $q'(y')$ of slab, proportional to depth of slab.

Fig. 7. Latitudinal profiles of specific enthalpy $e'(y')$ of slab.

Fig. 8. Latitudinal profiles of $e'(y')/q'(y')$. This ratio is proportional to the temperature difference $\vartheta$ between slab and lower layer.

Fig. 5 shows the zonal mass transport for the three cases. The striking fact is the tendency of the model to develop an equatorial countercurrent, embedded within equatorial currents. This is due to entrainment forcing as can be seen by inspection of Eqs. (4.5) and (4.6), but is nearly independent of the particular entrainment profile. We conclude, therefore, that the entrainment concept, together with the wind stress, is able to produce a fairly realistic latitudinal pattern of the zonal mass transport in the ocean surface layer. Since the present model is symmetric with respect to the equator, there should be a tendency of the actual ocean to generate an equatorial countercurrent in the Southern Hemisphere as well. There is, in fact, evidence for a Southern Hemispheric countercurrent in the Pacific Ocean (Reid, 1961) and in the Atlantic Ocean (Reid, 1964).

Fig. 6 shows for the three cases the distribution of specific mass which is proportional to the depth of the slab. The observed depth distribution of the mixed layer in the northern Pacific Ocean is characterized by a pronounced equatorial minimum and a maximum at 5° latitude; in the subtropics strong seasonal fluctuations prevail (Wyrtki, 1964). As a rule, the mixed layer is shallow in the inner tropics and deep in the subtropics (Defant, 1961, p. 120). The depth profiles of Fig. 6 are in accordance with this general picture.

In Fig. 7 the thermal energy, or the specific enthalpy of the slab with respect to the lower layer, is plotted as a function of latitude. The patterns are similar to the depth profiles. Evidence for low heat content of the slab in the equatorial region seems to be supported by satellite observations which show a relatively cloud-free equator (Kornfield et al., 1967). The latter statement can also be seen to follow from Fig. 8 which shows the ratio $e'(y')/q'(y')$. Combining Eqs. (4.5) and (4.8) yields

$$\frac{e'(y')}{q'(y')} = \int_0^y \zeta'(y')dy' / \int_0^y \sigma'(y')dy' \propto \vartheta_1. \quad (4.14)$$

The temperature difference between the slab and the lower layer is thus governed by the thermal heat input at the sea surface and the entrainment function; Fig. 8 exhibits a relatively cool equator and relatively warm subtropics.

5. Conclusions

This study has shown that an extremely simple model of an ocean surface slab gives a plausible description of some of the gross features of the oceanic surface circulation. In particular, the modeling of the equatorial countercurrent as a response to the combined action of wind stress and entrainment of cold water from below, as well as the depth distribution of the mixed layer and its latitudinal temperature pattern, may warrant interest. It seems that the concept of
entrainment velocity, first recognized by Rouse and Dodu (1955) in the laboratory, and further investigated and applied to oceanic conditions by Kraus and Turner (1967), and Yoshida (1967) is applicable to large-scale processes in the ocean. The present approach is different from thermoclinic methods. In models like the one-dimensional process by Overstreet and Rattray (1969), or the three-dimensional model of Niler and Dubbeldam (1970), the heat flux across the sea surface goes directly through the mixed layer to supply the heat flow required to maintain the thermocline. In the present model the entrainment function, instead of being determined by the divergence of the Ekman layer, is a mixing velocity; it is governed by the heat flux across the sea surface and the generation of turbulent kinetic energy due to wind stress and current shear. Keeping in mind the fairly low order of magnitude of the horizontal velocity (1 cm sec\(^{-1}\)), the response of this model should not be thought of as describing the actual surface circulation of the ocean very closely but rather as a significant baroclinic contribution to it.

If we assume that the temperature of the mixed layer is generally a smooth function of latitude, it follows from Eq. (4.14) that \( \sigma^e \) and \( \zeta^e \) must exhibit patterns that are not too different. If this conclusion is correct, it provides a means of estimating the entrainment function \( \sigma \) for which measurements are not yet available. It also shows the close correspondence between dynamic and energetic processes in the upper ocean in which most of the sun’s energy driving both oceanic and atmospheric motions is processed.

The latter viewpoint may have some implications for air-sea interaction models. There the driving forces of the present model are, in fact, interacting functions. In order to incorporate this, we can parameterize 1) the momentum exchange \( \tau \) between air and water by the surface wind stress, 2) the entrainment function \( \sigma \) in terms of the turbulent kinetic energy input and of the heat balance at the sea surface (Kraus and Turner, 1967), and 3) the net energy input \( \dot{q} \) into the ocean in terms of wind stress, sea surface temperature, and some atmospheric surface variables (see, e.g., Kraus and Rooth, 1961). According to these possible parameterizations, the present model can be extended to an hierarchy of models of increasing complexity.

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APPENDIX

List of Symbols

- \( a \) \hspace{1cm} \text{length parameter, } c_p/(\rho a)
- \( c_p \) \hspace{1cm} \text{specific heat per unit mass of water}
- \( e' \) \hspace{1cm} \text{nondimensional specific enthalpy}
- \( g \) \hspace{1cm} \text{earth’s acceleration}
- \( g' \) \hspace{1cm} \text{reduced earth’s acceleration}
- \( h_0 \) \hspace{1cm} \text{level of interface (“thermocline”) relative to reference level}
- \( h_1 \) \hspace{1cm} \text{thickness of slab}
- \( i \) \hspace{1cm} \text{index of interface between slab and lower layer}
- \( k \) \hspace{1cm} \text{linear friction constant}
- \( m' \) \hspace{1cm} \text{nondimensional zonal mass transport}
- \( m_n' \) \hspace{1cm} \text{nondimensional horizontal mass-transport vector}
- \( n' \) \hspace{1cm} \text{nondimensional meridional mass transport}
- \( p \) \hspace{1cm} \text{pressure}
- \( q' \) \hspace{1cm} \text{nondimensional specific mass}
- \( s \) \hspace{1cm} \text{index of sea surface}
- \( t \) \hspace{1cm} \text{time}
- \( t' \) \hspace{1cm} \text{nondimensional time}
- \( u \) \hspace{1cm} \text{zonal velocity component}
- \( v \) \hspace{1cm} \text{meridional velocity component}
- \( w' \) \hspace{1cm} \text{entrainment velocity}
- \( x \) \hspace{1cm} \text{zonal coordinate, positive eastward}
- \( y \) \hspace{1cm} \text{meridional coordinate, positive northward}
- \( y' \) \hspace{1cm} \text{nondimensional meridional coordinate}
- \( y^* \) \hspace{1cm} \text{meridional integration variable}
- \( z \) \hspace{1cm} \text{vertical coordinate, positive upward}
- \( D' \) \hspace{1cm} \text{scale of zonal wind stress}
- \( E \) \hspace{1cm} \text{specific enthalpy of slab}
- \( E' \) \hspace{1cm} \text{scale of specific enthalpy}
- \( Fr \) \hspace{1cm} \text{Froude number}
- \( H' \) \hspace{1cm} \text{scale of thickness of slab}
- \( M \) \hspace{1cm} \text{zonal mass transport}
- \( M' \) \hspace{1cm} \text{scale of horizontal mass transport}
- \( N \) \hspace{1cm} \text{meridional mass transport}
- \( P \) \hspace{1cm} \text{vertically integrated meridional pressure gradient}
- \( Q \) \hspace{1cm} \text{specific mass of slab}
- \( Q' \) \hspace{1cm} \text{scale of specific mass}
- \( Ro \) \hspace{1cm} \text{Rossby number}
- \( S' \) \hspace{1cm} \text{scale of entrainment mass flux}
- \( T' \) \hspace{1cm} \text{time scale of mass-transport equations}
- \( T_1' \) \hspace{1cm} \text{time scale of continuity and enthalpy equations}
\( Y' \) horizontal scale  
\( Z' \) scale of thermal energy input  
\( \alpha \) thermal expansion coefficient  
\( \beta \) meridional derivative of Coriolis parameter  
\( \gamma \) friction number  
\( \delta \) aspect ratio  
\( \epsilon \) Rossby number based on wind stress  
\( \xi \) thermal energy input  
\( \xi' \) nondimensional thermal energy input  
\( \vartheta \) nondimensional temperature  
\( \kappa \) nondimensional parameter  
\( \rho \) density  
\( \Delta \rho \) density difference between slab and lower layer  
\( \sigma \) entrainment mass flux  
\( \sigma' \) nondimensional entrainment mass flux  
\( \tau \) zonal wind stress plus integrated zonal pressure gradient  
\( \tau' \) nondimensional zonal wind stress  
\( \tau'_{x}, \tau'_{y} \) nondimensional horizontal wind stress vector  
\( \tau_{x}, \tau_{y} \) stress components at interface ("thermocline") level  
\( \Theta \) actual temperature

REFERENCES


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